Name:	NOTE: Hand in the exam!!	!

THE FINITE ELEMENT METHOD 2015 Dept. of Solid Mechanics

EXAMINATION: 2015-05-30

A maximum of 60 points can be obtained in this examination. To pass at least 30 points are required.

Permitted aid: Pocket calculator.

Problem 1: (12p)

The diffusion of Hydrogen molecules in a pressure vessel steel is modeled by the following parabolic partial differential equation

$$\frac{\partial c}{\partial t} = \operatorname{div}(\boldsymbol{M}\boldsymbol{\nabla}c) + s$$

with c the concentration field of Hydrogen molecules. M is the mobility of the Hydrogen molecules in steel and s a source of Hydrogen molecules. Both, M and s are given.

The boundary of the analyzed domain, V, is divided into one part S_h where $(\boldsymbol{M}\boldsymbol{\nabla}c)^T\boldsymbol{n}=h$ with h a given function on S_h and one part S_c where $(\boldsymbol{M}\boldsymbol{\nabla}c)^T\boldsymbol{n}=(d+f\,c)$ with d and f experimentally determined constants.

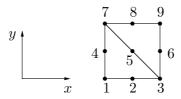
- a) Derive the weak form of the problem stated above.
- b) Derive the finite element formulation corresponding to the problem above. Note that you do not need to calculate any matrices.
- c) Suggest an element and show that the chosen element fulfills compatibility.

Problem 2: (12p)

The finite element formulation for two dimensional transient heat conduction takes the form

$$\left(\underbrace{\int_{A} \boldsymbol{N}^{T} c \rho \boldsymbol{N} dA}_{\boldsymbol{C}}\right) \dot{\boldsymbol{a}} + \left(\underbrace{\int_{A} \boldsymbol{B}^{T} \boldsymbol{D} \boldsymbol{B} dA}_{\boldsymbol{K}} + \underbrace{\int_{\mathcal{L}_{c}} \alpha \boldsymbol{N}^{T} \boldsymbol{N} d\mathcal{L}}_{\boldsymbol{K}}\right) \boldsymbol{a} = \underbrace{\int_{\mathcal{L}_{c}} \boldsymbol{N}^{T} \alpha T_{\infty} d\mathcal{L}}_{\boldsymbol{f}_{c}} - \underbrace{\int_{\mathcal{L}_{g}} \boldsymbol{N}^{T} q_{n} d\mathcal{L} - \int_{\mathcal{L}_{h}} \boldsymbol{N}^{T} h d\mathcal{L}}_{\boldsymbol{f}_{b}} + \underbrace{\int_{A} \boldsymbol{N}^{T} Q dA}_{\boldsymbol{f}_{b}}$$

where \mathcal{L}_c is the boundary where convection applies, \mathcal{L}_h is the boundary where the heat flow is prescribed and \mathcal{L}_g is the boundary where the temperature is prescribed.



The boundary conditions for the problem meshed by two 6-node triangular elements are

- Prescribed temperature at nodes 1-2-3, i.e. T = a = const.
- Prescribed heat flow trough the edge defined by the nodes 3-6-9, i.e. $q_n = h \neq 0$
- Convection at the edge defined by the nodes 1-4-7, i.e. $q_n = \alpha (T T_{\infty})$
- Insulated edge defined by the nodes 7-8-9, i.e. $q_n = 0$

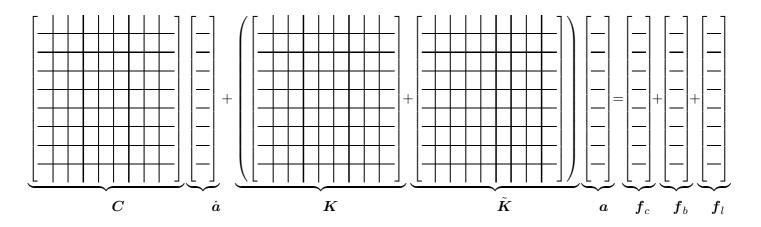
Additionally, heat is supplied via a constant heat source Q in the element defined by the nodes 3-6-9-8-7-5.

In the system of equations below mark

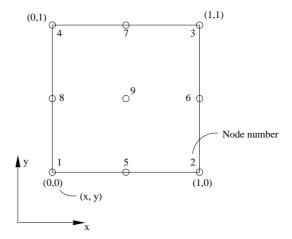
x – components that are known and different from zero

? – components that are unknown and different from zero

all blank positions are interpreted as zero.



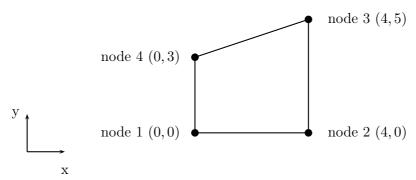
Problem 3: (12p)



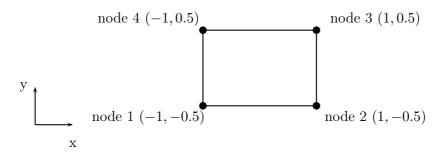
A nine-node Lagrange element (dimensions in mm) has been used in a two-dimensional elastic FE-analysis. On the boundary 4-7-3 there is a constant external force acting between (0.25,1)-(0.75,1). The force is due to friction and pressure and is given by $F_x = 5N$ and $F_y = -25N$. Calculate the contribution from F_x and F_y to the boundary load vector defined as $\mathbf{f}_b = \int_{\mathcal{L}} \mathbf{N}^T tt d\mathcal{L}$. The thickness t is 10mm.

Problem 4: (12p)

The isoparametric fully integrated four node element depicted below will be used in a thermal analysis.



- a) Determine the positions of the Gauss points, i.e. (x_i, y_i) for all four Gauss points.
- b) Another element is located as in the figure below. Calculate the integral $\int_A x^2 y^2 dA$ using full integration, i.e. four integration points.



Problem 5: (12p) FHLF10, Only Pi

The governing equations for a Bernoulli beam is given by

$$\frac{d^2M}{dx^2} + q = 0 \quad , \qquad M = -EI\frac{d^2w}{dx^2}$$

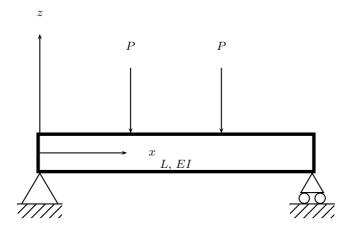
where q denotes the load intensity (positiv i z-direction). Note that the equilibrium equation is derived from the following relations

$$\frac{dM}{dx} = V \quad , \qquad \frac{dV}{dx} = -q$$

- a) Derive the weak form of the governing equation and specify the essential and natural boundary conditions.
- **b)** Derive the FE-formulation for the problem, such that a symmetric stiffness matrix is obtained.

c)

A beam is placed on two supports as shown in the figure below. The beam has the length L and bending stiffness EI. The beam is loaded with two forces of equal magnitude P at x = L/3 and x = 2L/3. Calculate the deflection at the center of the beam, i.e. at x = L/2.



Problem 5: (12p) FHLF01, Only F

The differential equation governing a column (simply supported in both ends) with an intial curvature is given by

$$\begin{aligned} \frac{d^2u}{dx^2} + \frac{1}{\pi^2}u + \sin x &= 0 \qquad 0 \le x \le \pi \\ u(0) &= u(\pi) &= 0 \end{aligned}$$

Make use of the following approximation

$$\bar{u}(x) = \sum_{k=1}^{n} a_k \sin(kx)$$

- 1. Determine the residual e(x).
- 2. Use the Galerkins method to determine the parameters $a_k, k = 1, 2, 3, ..., n$.

Hint:

$$\int_0^{\pi} \sin(kx)\sin(lx)dx = \begin{cases} 0 & \text{om } k \neq l \\ \pi/2 & \text{om } k = l \end{cases}$$

Some hints that might be helpful

Hint: Green-Gauss's theorem states:

$$\int_{A} \phi div \boldsymbol{q} dA = \oint_{\mathcal{L}} \phi \boldsymbol{q}^{T} \boldsymbol{n} d\mathcal{L} - \int_{A} (\boldsymbol{\nabla} \phi)^{T} \boldsymbol{q} dA$$

Hint: Some trigonometric relations:

$$\sin(\alpha)^{2} + \cos(\alpha)^{2} = 1$$

$$\sin(\alpha + \beta) = \sin(\alpha)\cos(\beta) + \cos(\alpha)\sin(\beta), \quad \cos(\alpha + \beta) = \cos(\alpha)\cos(\beta) - \sin(\alpha)\sin(\beta)$$

$$\sin^{2}(\alpha) = \frac{1 - \cos(2\alpha)}{2}, \quad \cos^{2}(\alpha) = \frac{1 + \cos(2\alpha)}{2}$$

$$\sin(2\alpha) = 2\sin(\alpha)\cos(\alpha), \quad \tan(2\alpha) = \frac{2\tan(\alpha)}{1 - \tan^{2}(\alpha)}$$

Hint: A quadratic matrix is positive semidefinite if

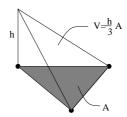
$$a^T K a \ge 0$$
, $\forall a$, and $a^T K a = 0$ for some $a \ne 0$

Hint: The interpolation formula of Lagrange is given by

$$l_k^{n-1} = \frac{(x-x_1)....(x-x_{k-1})(x-x_{k+1})....(x-x_n)}{(x_k-x_1)....(x_k-x_{k-1})(x_k-x_{k+1})....(x_k-x_n)}$$

Hint: Fourier's law is given by $q = -D\nabla T$

Hint:



Hint: The position, ξ_i , of the integration points and weights, H_i , for n number of integration points can be found from

$$\begin{array}{c|cc}
n & \xi_i & H_i \\
\hline
1 & 0 & 2 \\
2 & \pm 1/\sqrt{3} & 1
\end{array}$$

where integration from -1 to 1 is assumed.

Hint:

$$\begin{bmatrix} 1 & 0 & 0 \\ 1 & a & b \\ 1 & c & d \end{bmatrix}^{-1} = \frac{1}{ad - bc} \begin{bmatrix} (ad - bc) & 0 & 0 \\ -d + b & d & -b \\ c - a & -c & a \end{bmatrix}$$