Some examples

Principle of minimum energy - Discrete system systems

We have previously derived the equilibrium equations Ka = f for a system of springs based on equilibrium of the nodes. An alternative approach to derive the equilibrium equations can be found by considering the potential Π defined as

$$\Pi(\boldsymbol{a}) = W(\boldsymbol{a}) - \boldsymbol{a}^T \boldsymbol{F} \tag{1}$$

where $W = \frac{1}{2} \boldsymbol{a}^T \boldsymbol{K} \boldsymbol{a}$ is the stored energy of the system and $\boldsymbol{a}^T \boldsymbol{F}$ is referred to as the potential due to the external load. Note that in the definition of Π the external force \boldsymbol{F} is constant. Minimization of the potential Π implies that Π should be stationary and therefore

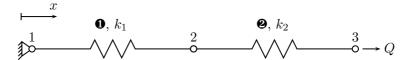
$$\frac{\partial \Pi}{\partial \{\boldsymbol{a}\}_i} = 0 \tag{2}$$

must hold, where $\{a\}_i$ represents the i:th component of a. Due to symmetry of the stiffness matrix this expression can be rewritten as

$$\frac{\partial \Pi}{\partial \{\boldsymbol{a}\}_i} = \sum_{j=1}^{ndof} \boldsymbol{K}_{ij} \boldsymbol{a}_j - \{\boldsymbol{F}\}_i = 0 \quad \forall i$$
 (3)

i.e. we have found that a minimization of the potential Π implies the equilibrium. In many textbook the principle of minimum energy is taken as the basis for the finite element formulation.

Let us now turn to the 'two-spring' example shown in Fig. 1. The total



Figur 1: Illustration of a two connected springs loaded in tension.

stored energy for this system is given as the sum of the stored energy in each spring. For spring 1 the elongation, Δ_1 , is equal to u_2 since $u_1 = 0$. For spring 2 the elongation, Δ_2 , is $\Delta_2 = u_3 - u_2$. The total stored energy can now be expressed as

$$W(u_2, u_3) = \frac{k_1 u_2^2}{2} + \frac{k_2 (u_3 - u_2)^2}{2}$$
(4)

Referring to (1) the total potential, Π , for the system can be written as

$$\Pi = W - Qu_3 = \frac{k_1 u_2^2}{2} + \frac{k_2 (u_3 - u_2)^2}{2} - Qu_3$$
 (5)

The minumum of Π is found by requiring $\frac{\partial \Pi}{\partial u_2} = 0$ and $\frac{\partial \Pi}{\partial u_3} = 0$, i.e.

$$\frac{\partial \Pi}{\partial u_3} = k_1 u_2 - k_2 (u_3 - u_2) = 0$$

$$\frac{\partial \Pi}{\partial u_3} = k_2 (u_3 - u_2) - Q = 0$$
(6)

These two equations can be written in matrix format as

$$\begin{bmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} \begin{bmatrix} u_2 \\ u_3 \end{bmatrix} \begin{bmatrix} 0 \\ Q \end{bmatrix}$$
 (7)

i.e. the minimium potential energy enable us to form Ka = f.

Principle of minimum energy - continous system

For an axially loaded bar the potential energy can be expressed as

$$\Pi = \underbrace{\int_0^L \frac{1}{2} A E \varepsilon^2 dx}_{W} - \int_0^L b u dx - [uN]_0^L$$
 (8)

where $\varepsilon = \frac{du}{dx}$. We shall now prove that a minimum to Π corresponds is an equilibruim solution. For this reason we assume that u is an equilibrium solution. If u minimizes the potential Π then $\Pi(u) \leq \Pi(u^*)$ or $\Pi(u) - \Pi(u^*) \leq 0$ for all choices of u^* . If we chose $u^* = u + v$ where v is a function that satisfies the essential boundary conditions if follows that u^* satisfies the essential boundary conditions. Using the definition for Π we obtain

$$\Delta\Pi(u, u^*) = \Pi(u) - \Pi(u^*) = \int_0^L \left(\frac{1}{2}AE\left(\frac{du}{dx}\right)^2 - \frac{1}{2}AE\left(\frac{du}{dx} + \frac{dv}{dx}\right)^2\right) dx$$
$$-\int_0^L budx - [uN]_0^L + \int_0^L b(u+v)dx + [(u+v)N]_0^L$$
(9)

Expansion and simplification of (9) results in

$$\Delta\Pi(u, u^*) = -\int_0^L \left(AE \left(\frac{dv}{dx} \frac{du}{dx} + \frac{1}{2} \left(\frac{dv}{dx} \right)^2 \right) \right) dx + \int_0^L bv dx + [vN]_0^L$$
(10)

Since u is an equilibrium solution it must satisfy the weak form. Using this result we conclude that

$$\Delta\Pi(u, u^*) = \Pi(u) - \Pi(u^*) = -\int_0^L AE \frac{1}{2} \left(\frac{dv}{dx}\right)^2 dx \le 0$$
 (11)

and we conclude that $\Pi(u) \leq \Pi(u^*)$, i.e. the displacement field that is minimizing the potential Π is soving the equlibrium.

Principle of minimum energy - General elasticity

Assume that a strain energy potential exsists, i.e. $w = w(\varepsilon)$ where $\varepsilon = \tilde{\nabla} u$. An obvious generalization of (8) reads

$$\Pi(\boldsymbol{u}^*) = \underbrace{\int_{\Omega} w dV}_{W} - \int_{\partial \Omega_t} \boldsymbol{t}^T \boldsymbol{u}^* dS$$
 (12)

where we require that u safisfies the essential boundary conditions. Suppose that u is a displacement field that satisfies equilibrium. In that case Π takes a minimal value for $\Pi(u)$. The minimization principle may be reformulated as

$$\Pi(\boldsymbol{u}) \le \Pi(\boldsymbol{u}^*), \quad \forall \boldsymbol{u}^*$$
 (13)

Let us now define u = tv where t is a scalar. Using this definition we can reformulate the minimization problem (13) as

$$\frac{d\Pi\left(\boldsymbol{u}+t\boldsymbol{v}\right)}{dt}|_{t=0}=0,\quad\forall\boldsymbol{v}$$
(14)

Let is now assume that the material is linear elastic, i.e.

$$w = \frac{1}{2} \boldsymbol{\varepsilon}^T \boldsymbol{D} \boldsymbol{\varepsilon} \tag{15}$$

where $\varepsilon = \varepsilon(u)$. Using (12), (14) and (15) we obtain

$$\frac{d\Pi\left(\boldsymbol{u}+t\boldsymbol{v}\right)}{dt}|_{t=0} = 0 =$$

$$\frac{d}{dt}|_{t=0} \left\{ \int_{\Omega} \frac{1}{2} \left(\tilde{\boldsymbol{\nabla}}(\boldsymbol{u}+t\boldsymbol{v}) \right)^{T} \boldsymbol{D} \left(\tilde{\boldsymbol{\nabla}}(\boldsymbol{u}+t\boldsymbol{v}) \right) dV - \int_{\partial\Omega_{t}} \boldsymbol{t}^{T}(\boldsymbol{u}+t\boldsymbol{v}) ds \right\}$$
(16)

After expaning the terms in (16) and using $D = D^T$ we obtain

$$\int_{\Omega} \left(\tilde{\boldsymbol{\nabla}} \boldsymbol{v} \right)^{T} \boldsymbol{D} \left(\tilde{\boldsymbol{\nabla}} \boldsymbol{u} \right) dV - \int_{\partial \Omega_{t}} \boldsymbol{t}^{T} \boldsymbol{v} ds = \boldsymbol{0}$$
(17)

which we recognize as the weak form of the equilibrium equations and we can, again, conclude that minimization of the potential Π results in the weak form