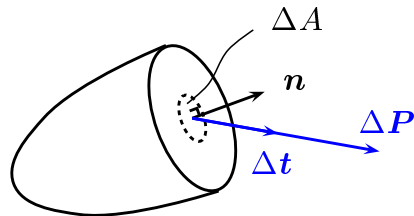


TRACTION VECTOR



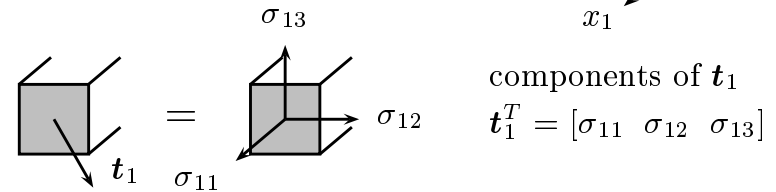
Let us define

$$t_i = \lim_{\Delta A \rightarrow 0} \frac{\Delta P_i}{\Delta A}$$

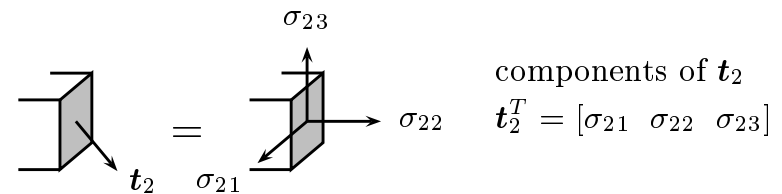
traction vector

STRESS COMPONENTS

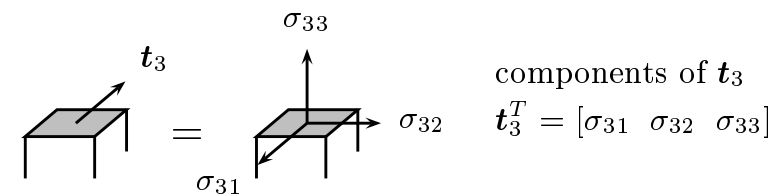
Choose $\mathbf{n}^T = [1 \ 0 \ 0]$ $\Rightarrow \mathbf{t} = \mathbf{t}_1$



Choose $\mathbf{n} = [0 \ 1 \ 0]$ $\Rightarrow \mathbf{t} = \mathbf{t}_2$



Choose $\mathbf{n} = [0 \ 0 \ 1]$ $\Rightarrow \mathbf{t} = \mathbf{t}_3$

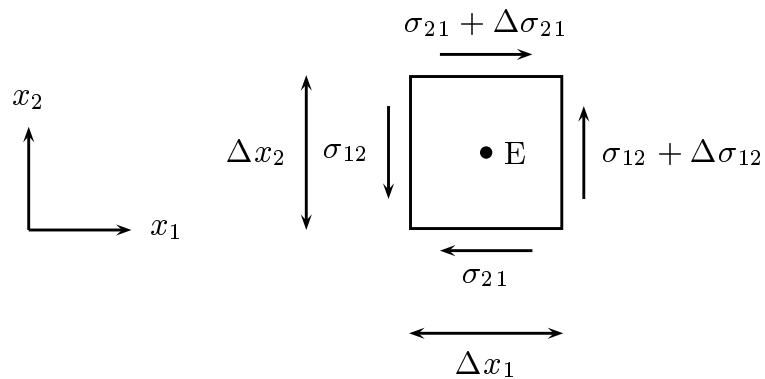


Define stress tensor

$$\sigma_{ij} = \begin{bmatrix} \mathbf{t}_1^T \\ \mathbf{t}_2^T \\ \mathbf{t}_3^T \end{bmatrix} = \begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix}$$

PROPERTIES OF σ_{ij}

Moment equilibrium



Moment about E

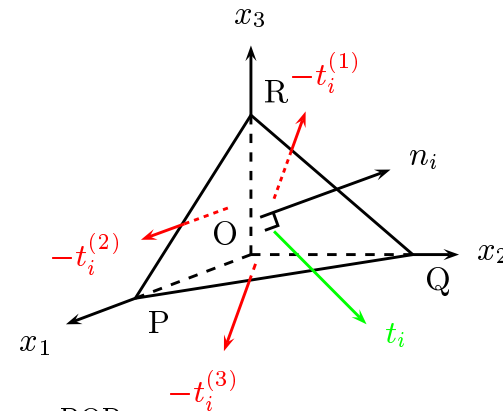
$$\sigma_{12} = \sigma_{21}$$

In general

$$\sigma_{ij} = \sigma_{ji}$$

symmetric

PROPERTIES OF σ_{ij}



$$dS = \text{area PQR}$$

$$dS_1 = \text{area ROQ}$$

$$dS_2 = \text{area POR}$$

$$dS_3 = \text{area POQ}$$

Equilibrium

$$t dS - t_1 \underbrace{dS_1}_{=n_1 dS} - t_2 \underbrace{dS_2}_{=n_2 dS} - t_3 \underbrace{dS_3}_{=n_3 dS} + b dV = 0$$

$$\Rightarrow t - \underbrace{t_1 n_1 - t_2 n_2 - t_3 n_3}_{-\sigma^T \mathbf{n}} + b \underbrace{\frac{dV}{dS}}_{\rightarrow 0} = 0$$

$$t_i = \sigma_{ij} n_j$$

Cauchy's formula
exactly what we wanted!

PROPERTIES OF σ_{ij}

We found

$$t_i = \sigma_{ij} n_j$$

In another coordinate system

$$t'_i = \sigma'_{ij} n'_j$$

t_i and n_i are vectors (first-order tensors)

Use transformation rules for t_i and n_i

⇒

$$\begin{aligned} \sigma'_{ij} &= A_{ik} \sigma_{kl} A_{jl} & \text{or} & & \boldsymbol{\sigma}' &= \mathbf{A} \boldsymbol{\sigma} \mathbf{A}^T \\ \sigma_{ij} &= A_{ki} \sigma'_{kl} A_{lj} & \text{or} & & \boldsymbol{\sigma} &= \mathbf{A}^T \boldsymbol{\sigma}' \mathbf{A} \end{aligned}$$

$$\sigma_{ij} = \text{second-order tensor}$$

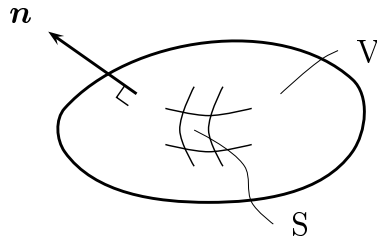
PROPERTIES OF σ_{ij}

In analogy with the strain tensor we obtain

- Mohr's circle's of stress
- Principal stress - principal directions
- Invariants
- Cayley-Hamilton's theorem
- Deviatoric stress tensor

$$\begin{aligned} s_{ij} &= \sigma_{ij} - \frac{1}{3} \delta_{ij} \sigma_{kk} \\ s_{kk} &= 0 \end{aligned}$$

DIVERGENCE THEROREM OF GAUSS



n = outer unit normal vector

c = arbitrary vector; $\mathbf{c}^T = [c_1 \ c_2 \ c_3]$

Divergence theorem

$$\int_S \mathbf{c}^T \mathbf{n} dS = \int_V \text{div} \mathbf{c} dV$$

where

$$\text{div} \mathbf{c} = \frac{\partial c_1}{\partial x_1} + \frac{\partial c_2}{\partial x_2} + \frac{\partial c_3}{\partial x_3} = c_{j,j}$$

$$\mathbf{c}^T \mathbf{n} = c_j n_j$$

$$\Rightarrow \int_S c_j n_j dS = \int_V c_{j,j} dV$$

Generalization

$$\int_S c_{ij} n_j dS = \int_V c_{ij,j} dV$$

EQUATIONS OF MOTION

We found

$$\int_S c_{ij} n_j dS = \int_V c_{ij,j} dV$$

Newton's second law

$$\int_S t_i dS + \int_V b_i dV = \int_V \rho \ddot{u}_i dV$$

\uparrow traction vector \uparrow body force \nwarrow acceleration

We have

$$\int_S t_i dS = \int_S \sigma_{ij} n_j dS = \int_V \sigma_{ij,j} dV$$

$$\int_V (\sigma_{ij,j} + b_i - \rho \ddot{u}_i) dV = 0$$

Volume V is arbitrary \Rightarrow

$$\sigma_{ij,j} + b_i = \rho \ddot{u}_i$$

equations of motion

WEAK FORM - PRINCIPLE OF VIRTUAL WORK

Equations of motion

$$\sigma_{ij,j} + b_i = \rho \underbrace{\ddot{u}_i}_{\text{acceleration}}$$

Multiply with v_i and integrate of volume

$$\int_V v_i (\sigma_{ij,j} + b_i - \rho \ddot{u}_i) dV = 0$$

v_i = arbitrary weight vector

Use of divergence theorem and Cauchy's formula

$$(t_i = \sigma_{ij} n_j) \Rightarrow$$

$$\int_V \rho v_i \ddot{u}_i dV + \int_V \underbrace{v_{i,j} \sigma_{ij}}_{\epsilon_{ij}^v \sigma_{ij}} dV = \int_S v_i t_i dS + \int_V v_i b_i dV$$
$$\epsilon_{ij}^v = \frac{1}{2} (v_{i,j} + v_{j,i})$$